

“The Laser Microengineering Experimental Station” at the Jefferson Laboratory Free Electron Laser Facility

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LPC 2004

Project Goals

- **Establish a working facility that will enable user-friendly application of the unique FEL properties for investigations in laser microengineering science and laser material processing technology development.**
- **Effort delineated into two segments.**
 - **Build**
 - an engineering model and process development station at The Aerospace Corporation - called Aerospace-Engineering Model (A-EM)
 - a working model at the Jefferson FEL - called JLAB-working Model (JLAB-WM)
 - **Operate**
 - transition newly developed laser processes and techniques,
 - conducting fundamental investigations in laser material interaction phenomenon,
 - assisting/guiding new users.

Examples of laser microengineering possible

- **Multi-color direct-write microfabrication**
- **Volumetric exposure, multi-photon exposure processing**
- **Percussion machining, ablative machining**
- **Polishing**
- **Chemical vapor deposition (with special cell)**
- **Crystallization**
- **Micro-fusing**
- **Surface texturing**
- **Investigations: Laser material interaction phenomena**
- **Mass & optical spectroscopy of desorption and ablation**
- **Mass removal rate measurement**
- **Pump-probe physics**
- **Multiple pulse - rep-pulse physics**
- **Small Scale Pulsed Laser Deposition (PLD)**

System Attributes

- A laser beam delivery system for processing in the UV and IR.
- Automated sequencing of tool changes (e.g. color, objective).
- User selects from three focusing objectives.
- A coordinated three-axis motion system, XY motion range of 100mm.
- An optical table with integrated vibration isolation capability.
- An automated means for laser power and repetition rate control.
- A vision system for process control.
- A means for the User to measure the laser spot size & intensity distribution.
- CAD software for solid modeling of patterns.
- CAM software for generating 3 axes tool-path.
- Software for visual verification of the tool-path geometry.
- Software for converting the tool-path geometry into motion language.
- A generic scheme for mounting user supplied sample holders.
- An enclosure that can be interlocked with JLAB FEL safety systems.
- Additional laser beam delivery lines & stations for other experiments.

Designing for Vibration Control

Motion System is the Primary
“Vibration” Noise Source

Approach

Apply a Multi-tiered Solution to Vibration Control
Apply FEM Methods to Articulate Geometries that
Enhance Stiffness

Recommended by Aerotech to use solid granite table and solid granite “bridge/superstructure” for z-drive mounting

- All tapped-hole locations pre-specified
- Very heavy
- Claimed granite was ideal for *stiffness*
- Granite has same specific stiffness as steel
- Geometry has strong affect on stiffness

Weight 12,000 lbs

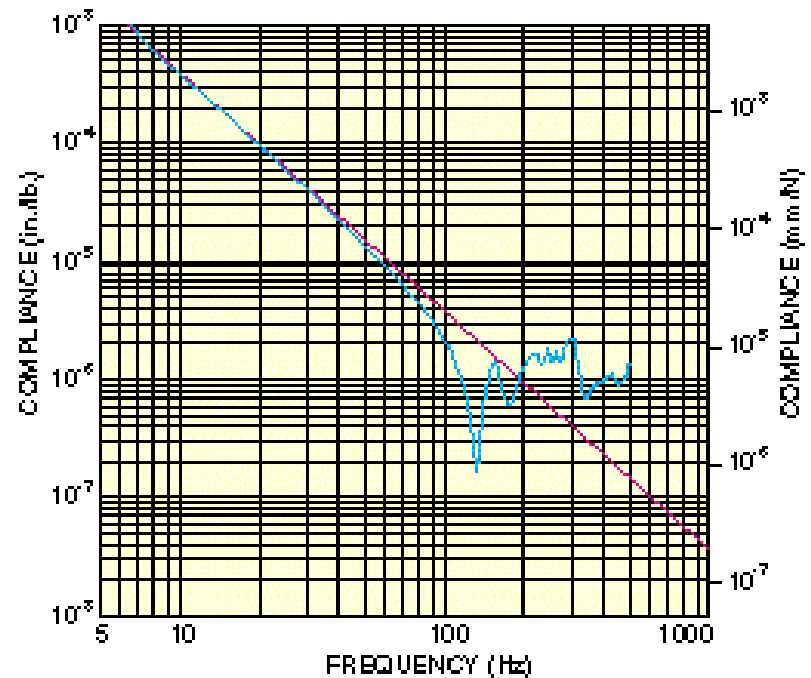


Newport RS 4000 Tables

Maximum Amplification
at a Resonance (Q)

Steel Honeycomb Core:
 $Q = 1.1 \times 10^{-5} / 3 \times 10^{-6} \sim 4$

Granite Block:
 $Q = 2.3 \times 10^{-4} / 5 \times 10^{-7} = 460$



Worst Case Relative Motion Value (RM)
 $RM = 2g(1/32\pi^3)^{1/2} (Q/f^3)^{1/2} (PSD)^{1/2} T$

For $Q = 1$, $f = 160$ Hz, $PSD^* = 10^{-5} \text{ g}^2/\text{Hz}$, $T = 0.01$

$$RM = 10 \text{ nm}$$

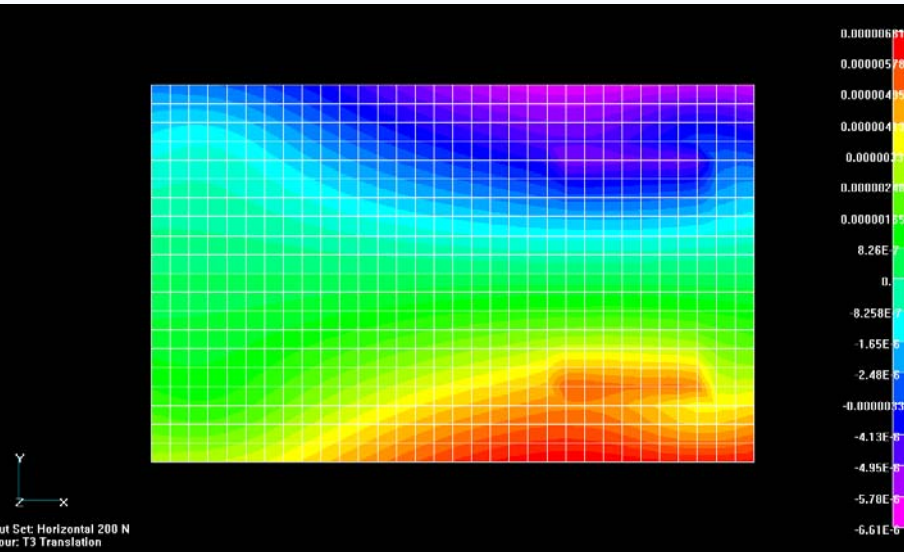
* PSD value is 10^4 times the PSD vibration found in a light manufacturing factory

Static Deflection (SD)
 $SD = (PL^3/24EbTH^2) + (PL/4GHb)$

For $P = 1000$ lbs, $L = 52''$, $b = 60''$
and $H = 12''$, $T = 0.1875''$,
 $E = 29 \times 10^6$ psi, $G = 2.25 \times 10^5$ psi

$$SD \sim 3.2 \times 10^{-4}'' \text{ (} 8 \text{ } \mu\text{m)}$$

FEM of table top: Static deflections



Vertical deflection due to horizontal load

Applied Force

Deflection

100 N

0.084 microns

200 N

0.17 microns

1100 N

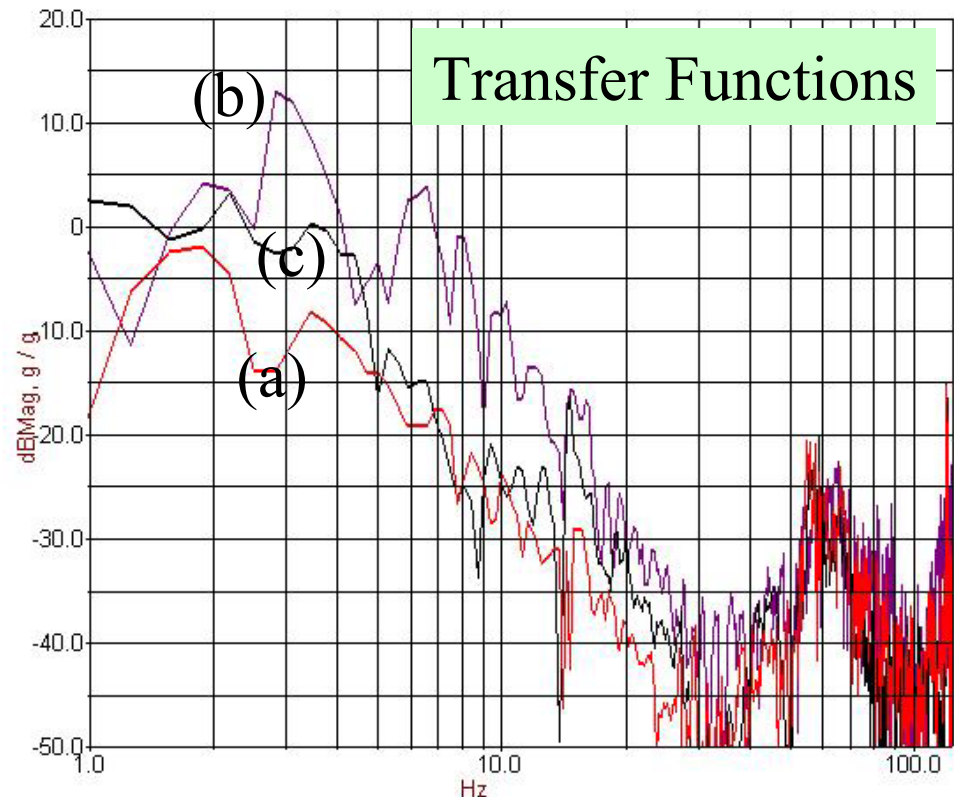
0.92 microns

Isolation System Design

Multi-tiered Approach

1. Pneumatic isolation (a)
2. + Elastomeric isolation (b)
3. + Magnetic-active isolation (c)

Working isolation system with enhanced rigidity

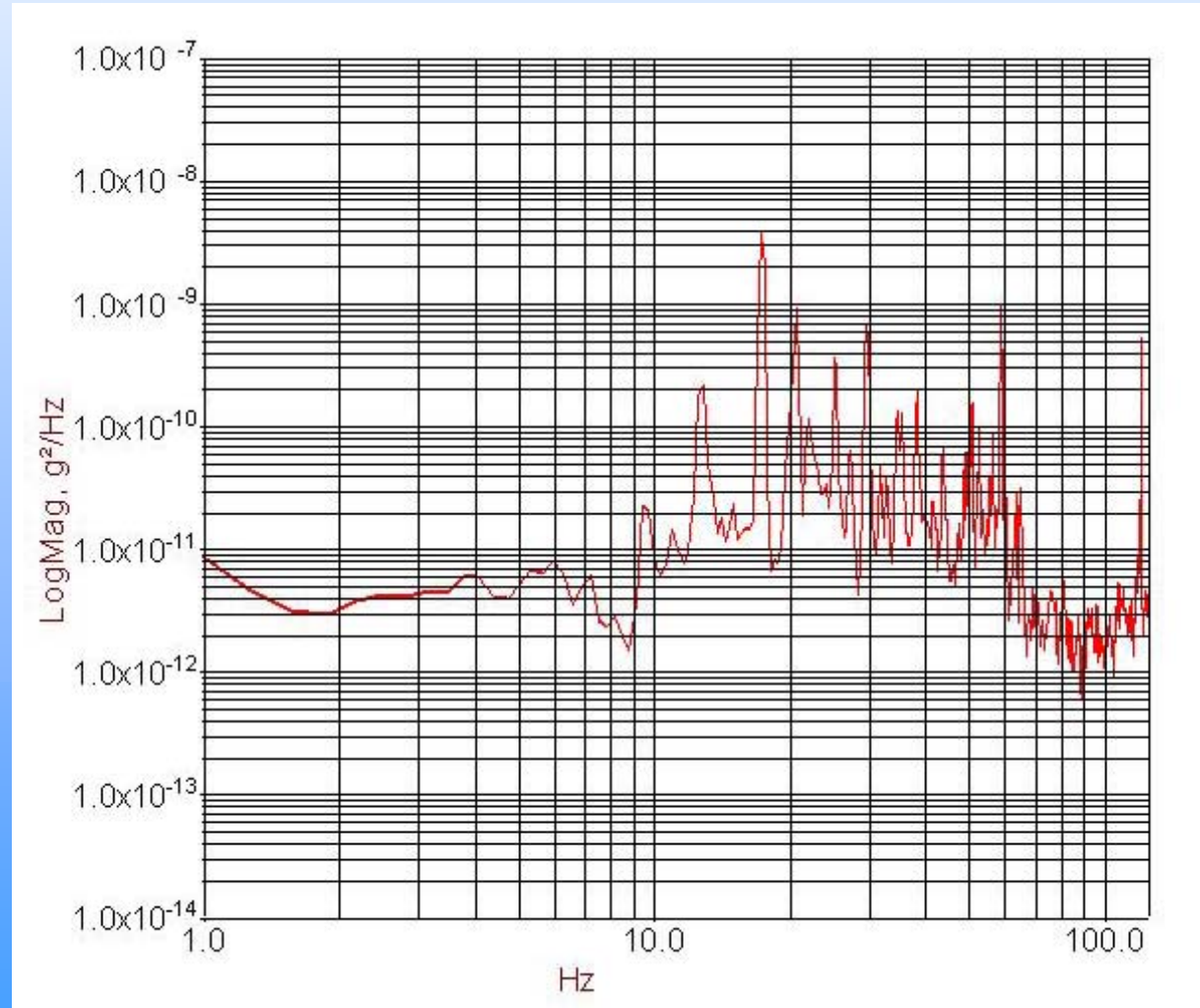


Measure Aerospace Lab Floor Noise for baseline

Power Spectral
Density Values

10^{-9} considered a
Quite Laboratory

10^{-8} Light
Manufacturing

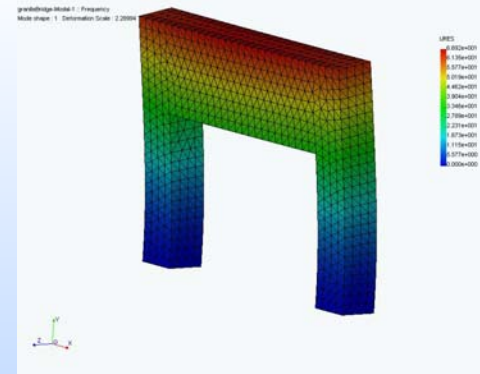


The SuperStructure

Legs 8" square

1209.08 lbm

Modes:	1	49.77 Hz
	2	110.55 Hz
	3	129.42 Hz

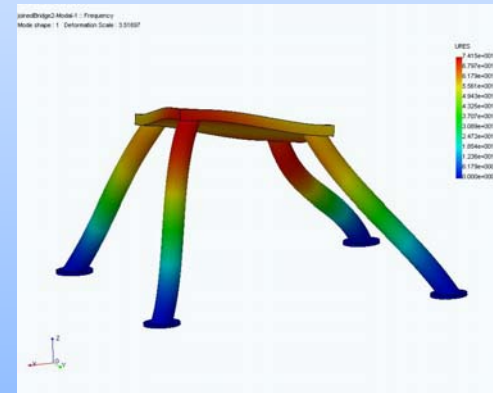


Legs 4" OD, 1/8" wall

324.65 lbm

Modes:	1	64.95 Hz
	2	64.95 Hz
	3	96.65 Hz

- 1/4" wall: 645 lb, 73 Hz

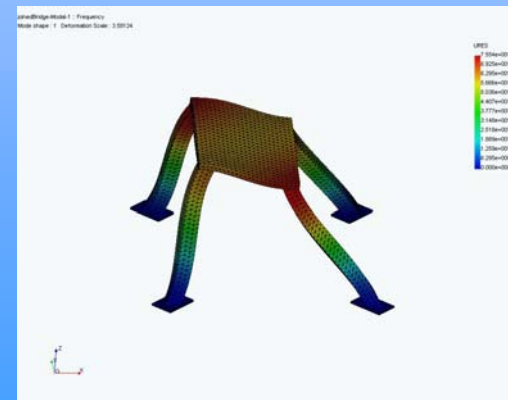


Legs 4" square, 1/8" wall

317.42 lbm

Modes:	1	84.03 Hz
	2	84.03 Hz
	3	127.28 Hz

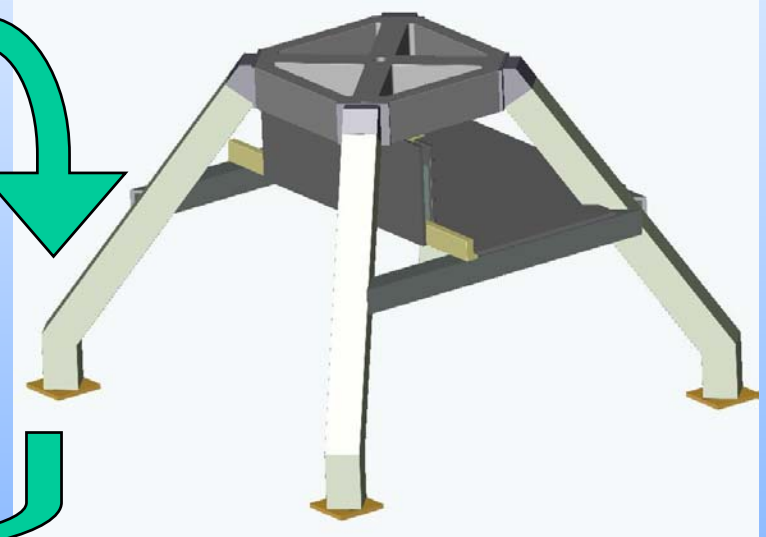
- 1/4" wall: 630 lb, 101 Hz



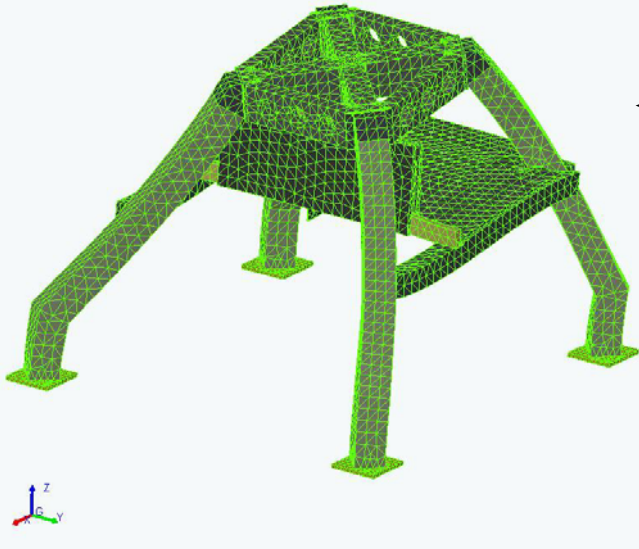
First Design of Support Structure



Evolved Design



Model name: assembledBridgeSqBntLeg
Study name: freq1
Plot type: Frequency Deformation - Plot1
Mode shape: 1 Value = 99.172 Hz
Deformation Scale 1: 2.74885



1107.23* lbm, Alloy Steel

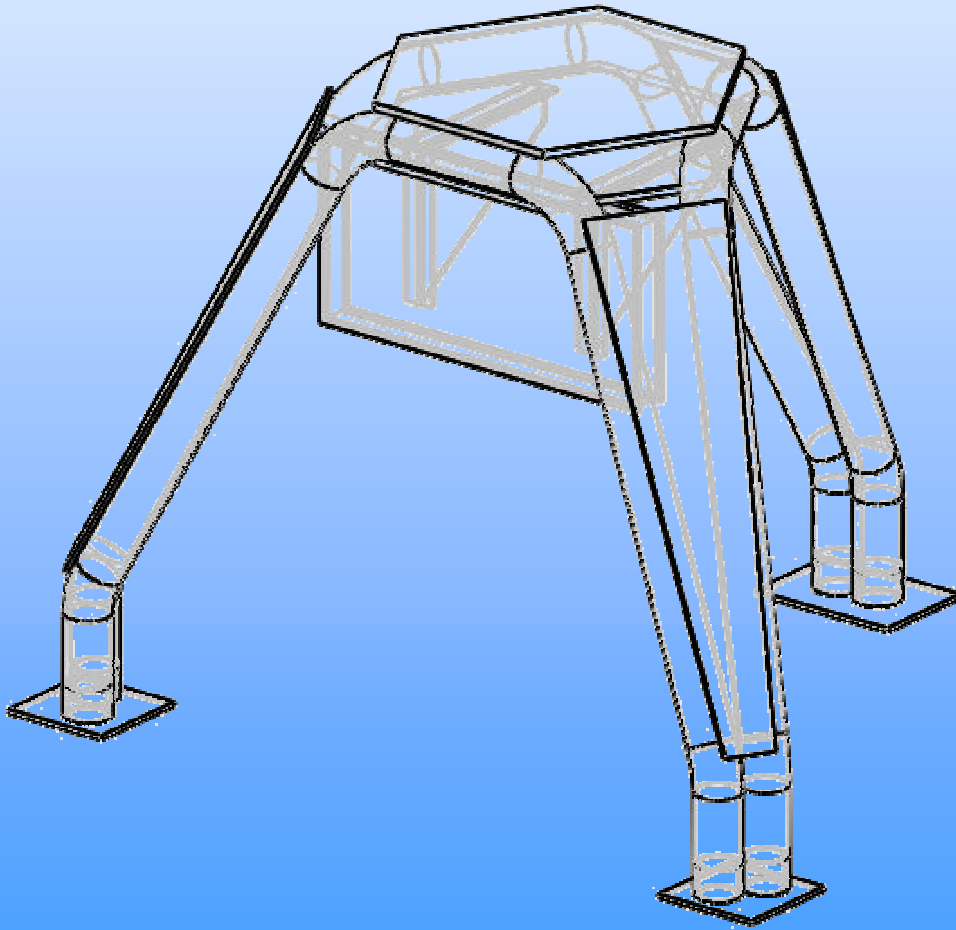
Mode 1: 100.66 Hz

Mode 2: 100.84 Hz

Mode 3: 137.12 Hz

*No Breadboard or vertical-mounted mass

Alternative Design 1 “Tripod”



Tripod Initial Results

Legs 3" OD, 1/8" thick

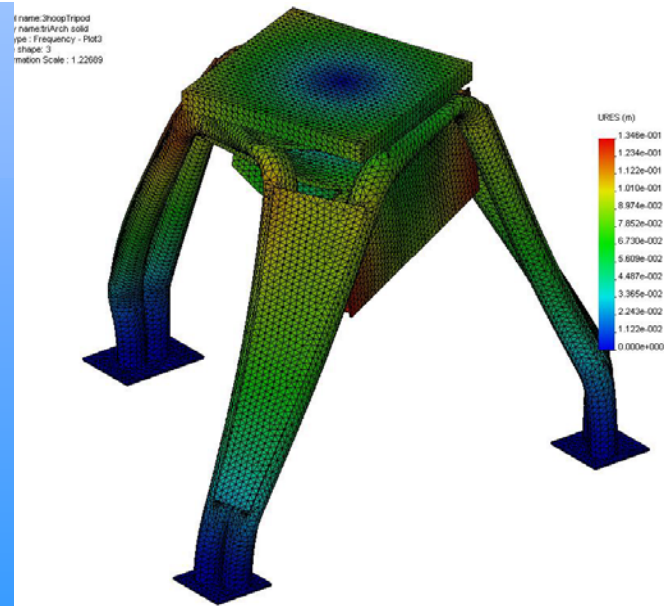
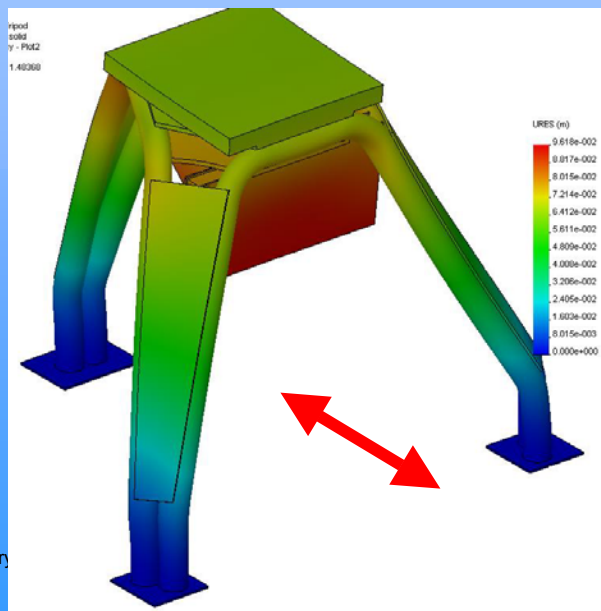
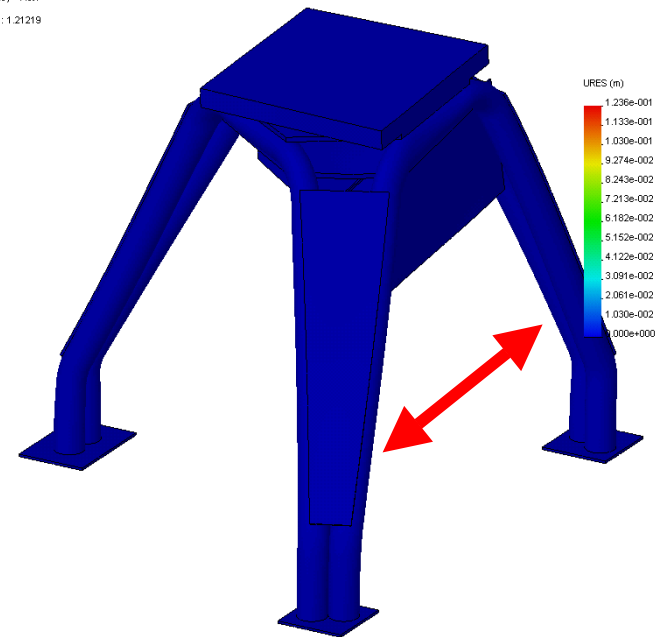
506.32 lbm (includes breadboards)

Modes:	1	57.157 Hz
	2	57.919 Hz
	3	117.13 Hz
	4	180.74 Hz
	5	204.47 Hz

* Solid elements, tetrahedral

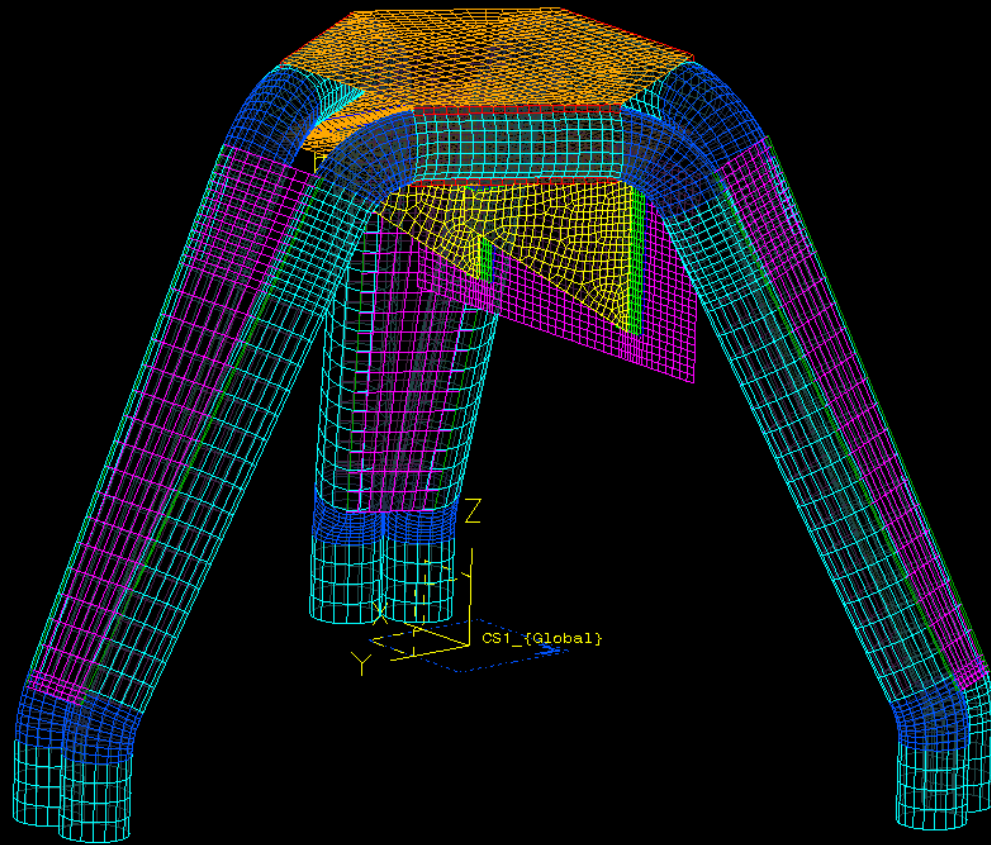
107,963 elements, 199,784 nodes

Model name: 3hoopTripod
Study name: triArch solid
Plot type: Frequency - Plot1
Mode shape: 1
Deformation Scale: 1.21219



4" OD legs, 1/16" thick

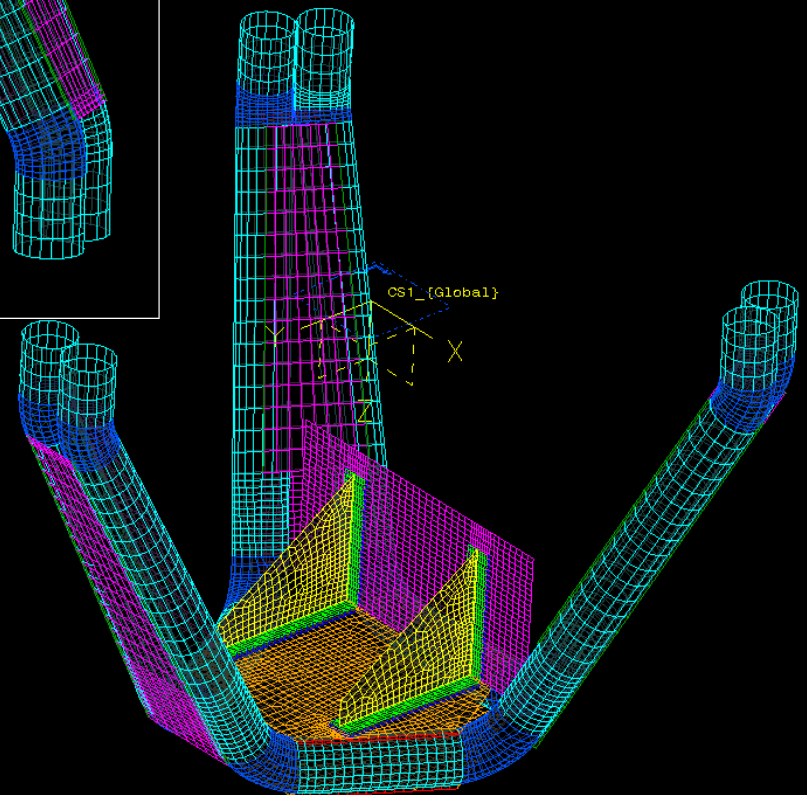
Requires shell elements, switch
from CosmosWorks to NASTRAN



Shell mesh quadrilateral elements

Elastic elements for welds

Ideas preprocessor/mesher



Tripod Analysis and Results

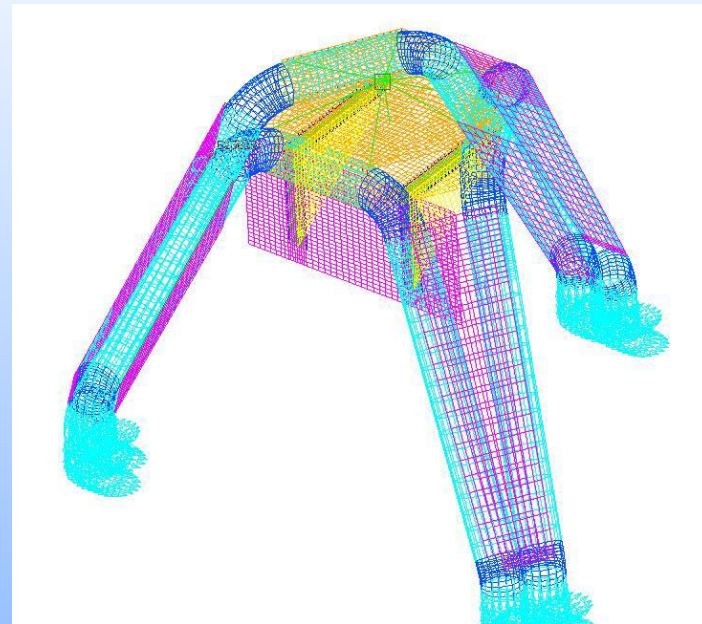
NASTRAN (MSC) solver

Ideas postprocessor/viewer

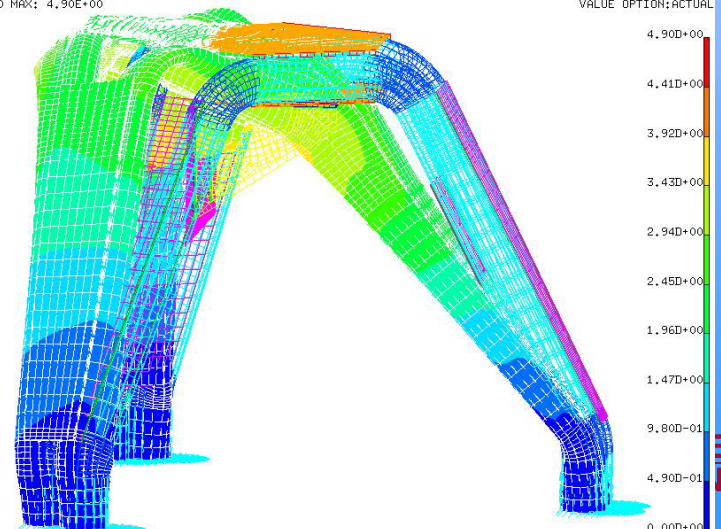
- 200 lbm point mass at CG of breadboard
- Rigid elements constraints to mounting plate
- 40 lbm breadboard + 15 lbm z-stage added
- Smeared properties for vertical breadboard
- Immovable restraints on bottom of leg, no feet

471.97 lbm (including breadboards & z stage)
First mode at **40 Hz**

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```
RESULTS: 1- B.C. 1,NORMAL_MODE 1,DISPLACEMENT_1  
MODE: 1 FREQ: 40.01566  
DISPLACEMENT - MAG MIN: 0.00E+00 MAX: 4.90E+00  
DEFORMATION: 1- B.C. 1,NORMAL_MODE 1,DISPLACEMENT_1  
MODE: 1 FREQ: 40.01566  
DISPLACEMENT - MAG MIN: 0.00E+00 MAX: 4.90E+00  
FRAME OF REF: PART
```



Tripod Design Iteration

Plate gussets were added to stiffen bent joints

Front plate less than 0.5" blocking of breadboard

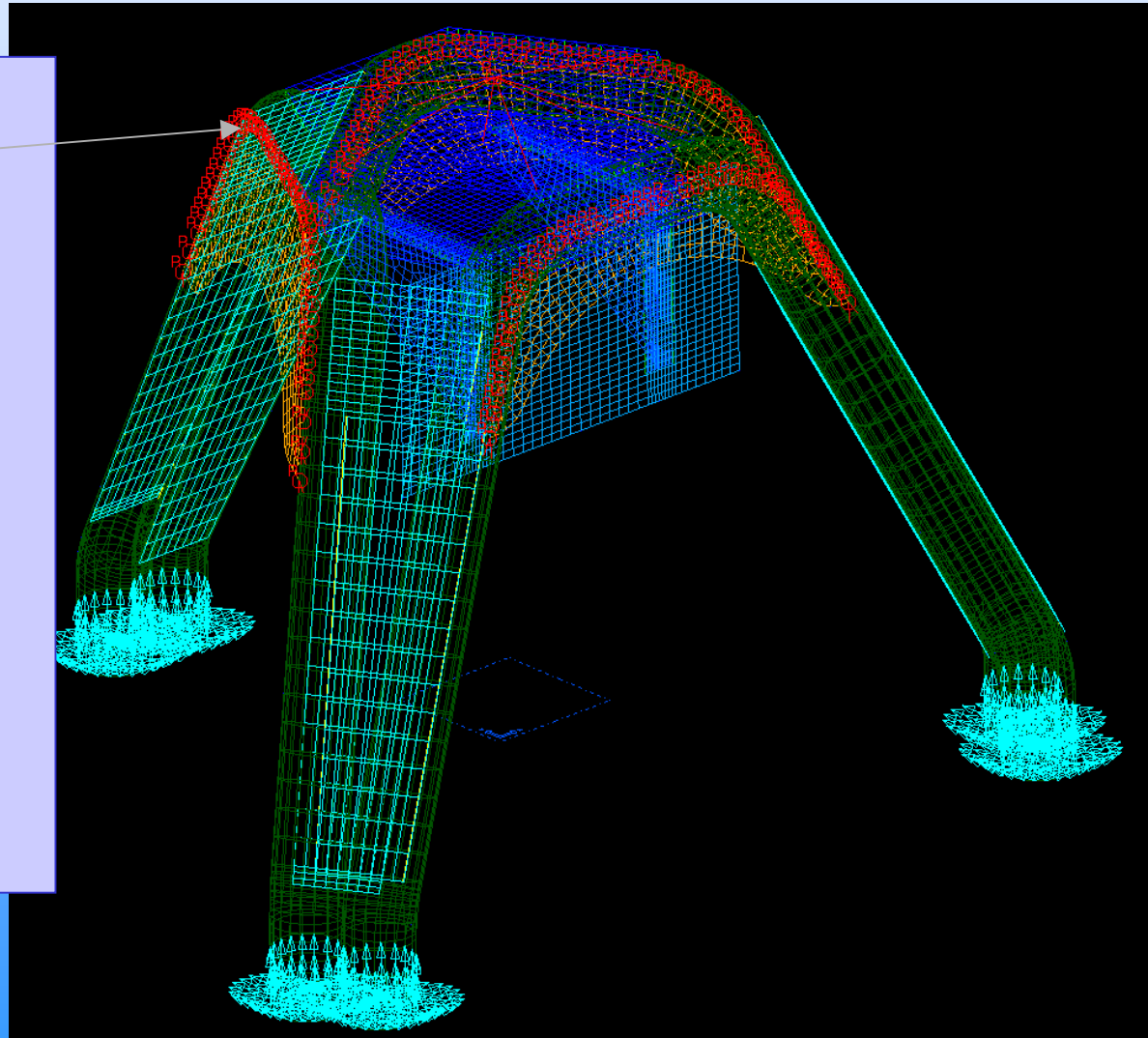


Analysis of New Tripod

Meshed gusset plates
separately
Connected by rigid
elements

Analysis performed
varying

Leg thickness
Gusset thickness
Geometry
combinations



First Mode: Swaying 78 Hz

I-DEAS Visualizer

Frame 1 of 8

Display 1

Modal

SUB ID=1,MODE=1,F=78.399HZ->MODE SHAPE

TITLE = LASER TRIPOD

DISPLACEMENT Magnitude Unaveraged Top shell

Min: 0.00E+00 in Max: 1.70E+00 in

SUB ID=1,MODE=1,F=78.399HZ->MODE SHAPE

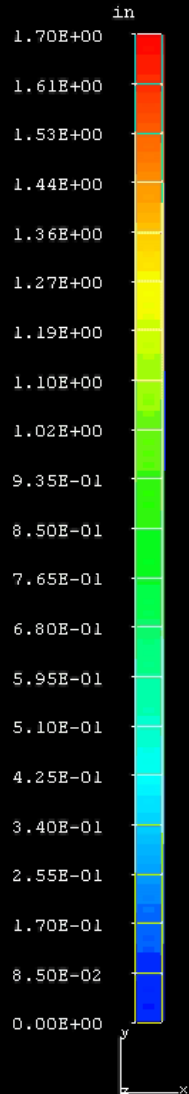
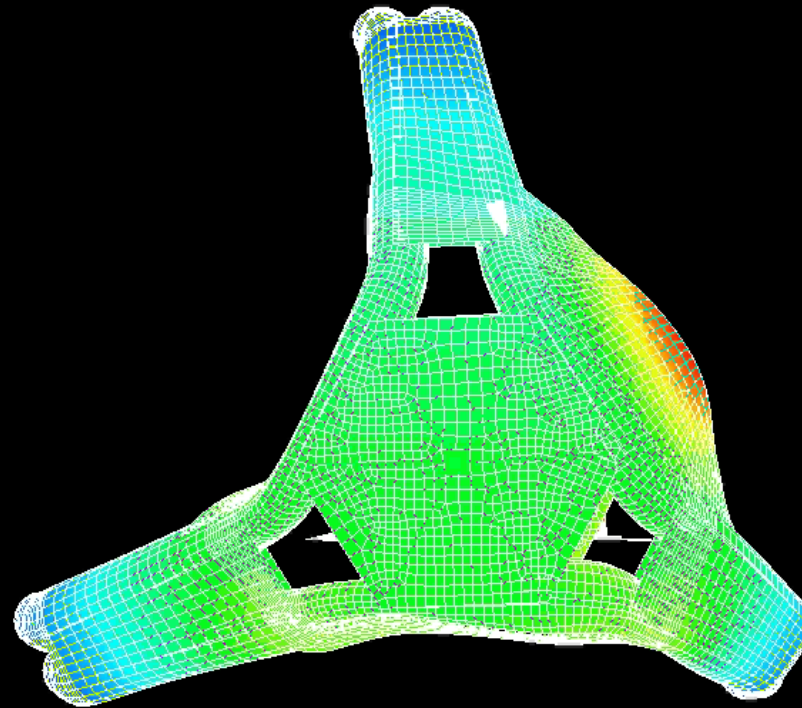
TITLE = LASER TRIPOD

DISPLACEMENT XYZ Magnitude

Min: 0.00E+00 in Max: 1.70E+00 in

Part Coordinate System

Frequency: 7.84E+01 Hz

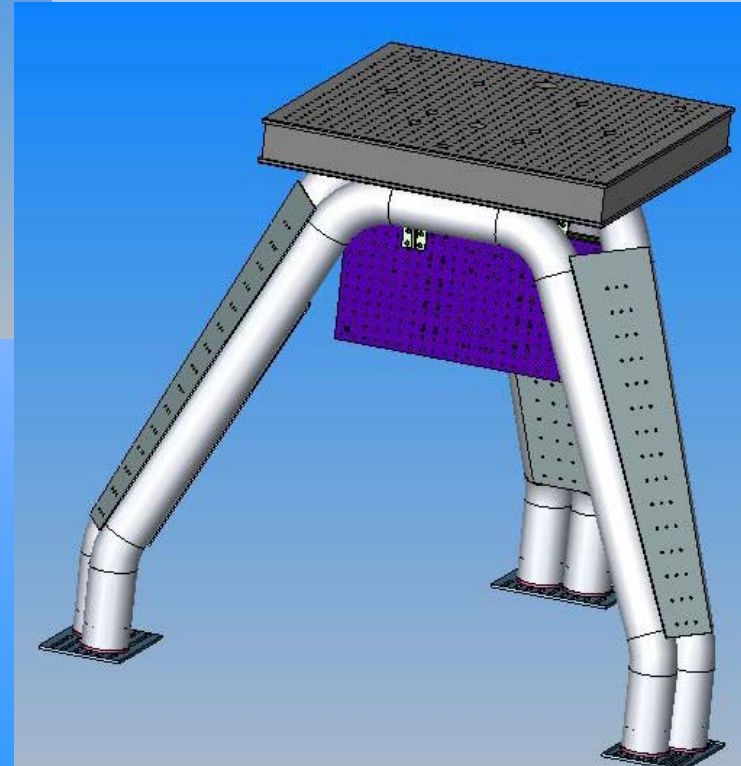
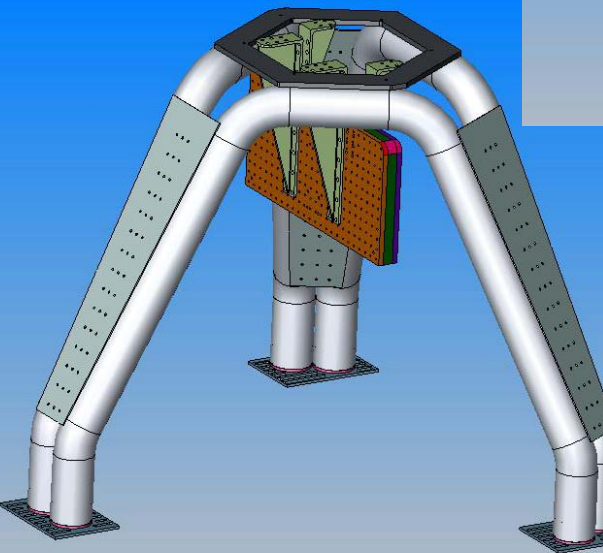
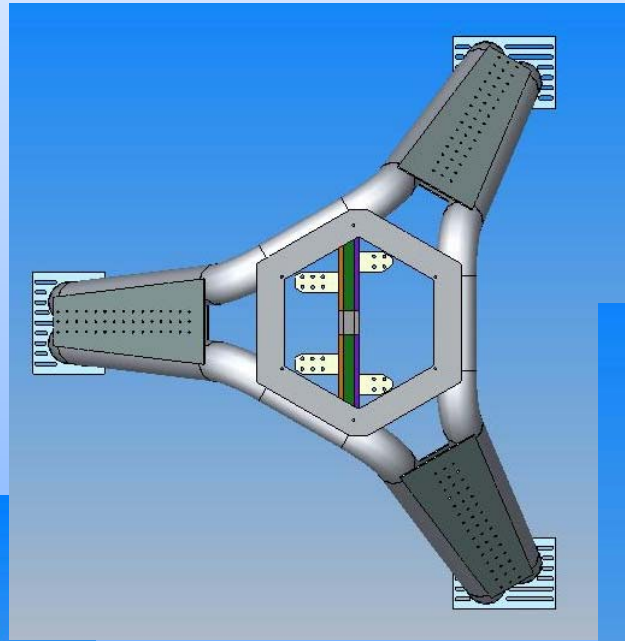


Summary of Analysis Results

	Baseline (1/16" Legs)	1/8" Legs	1/16" Legs + 3/16" Gusset	1/16" Legs + 1/4" Gusset	1/8" Legs + 3/16" Gusset
Mass (lbm)	471.97	534.43	496.52	504.70	558.97
Mode #					
1	39.77	60.39	57.76	58.71	78.40
2	41.00	62.31	63.93	64.70	84.98
3	87.81	109.23	92.09	92.66	112.03
4	102.91	143.72	124.49	126.44	156.18
5	121.12	157.75	132.67	139.12	177.69
6	141.76	217.76	137.94	145.99	179.64
7	166.65	246.62	156.83	158.19	200.99
8	228.80	333.08	160.46	160.68	233.63
9	230.26	339.03	184.82	188.93	256.93
10	231.06	340.48	203.29	222.64	265.52

Problem: Too costly to manufacture
 “one more try in analysis to refine design”

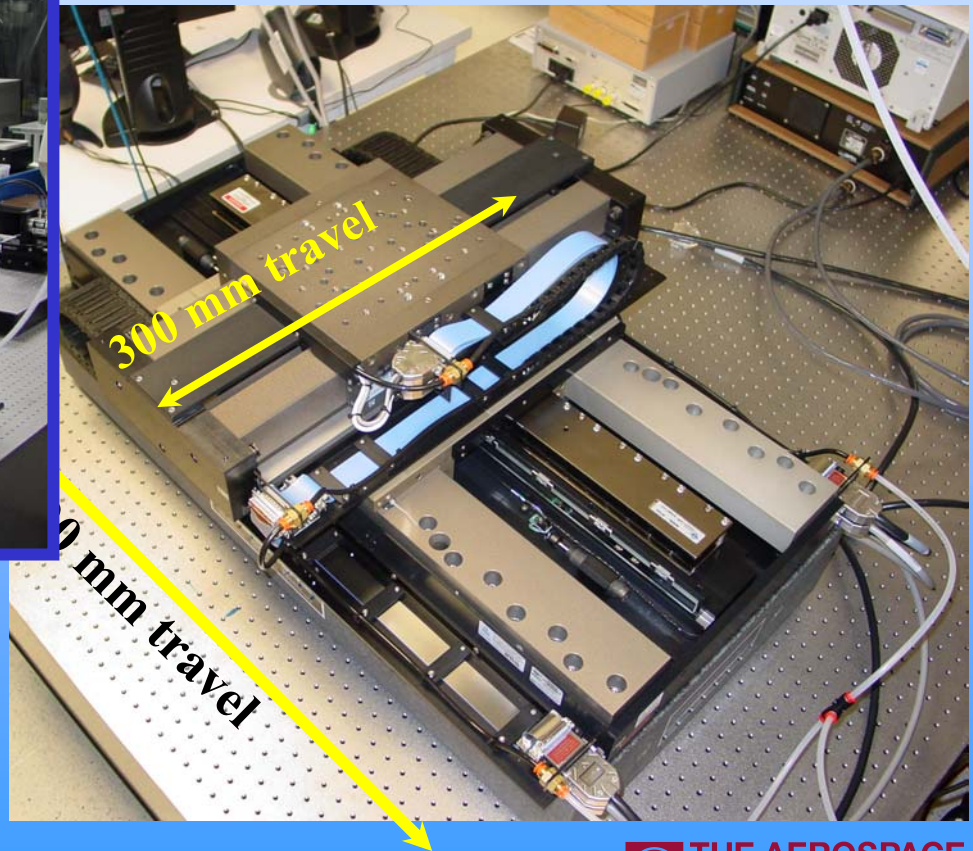
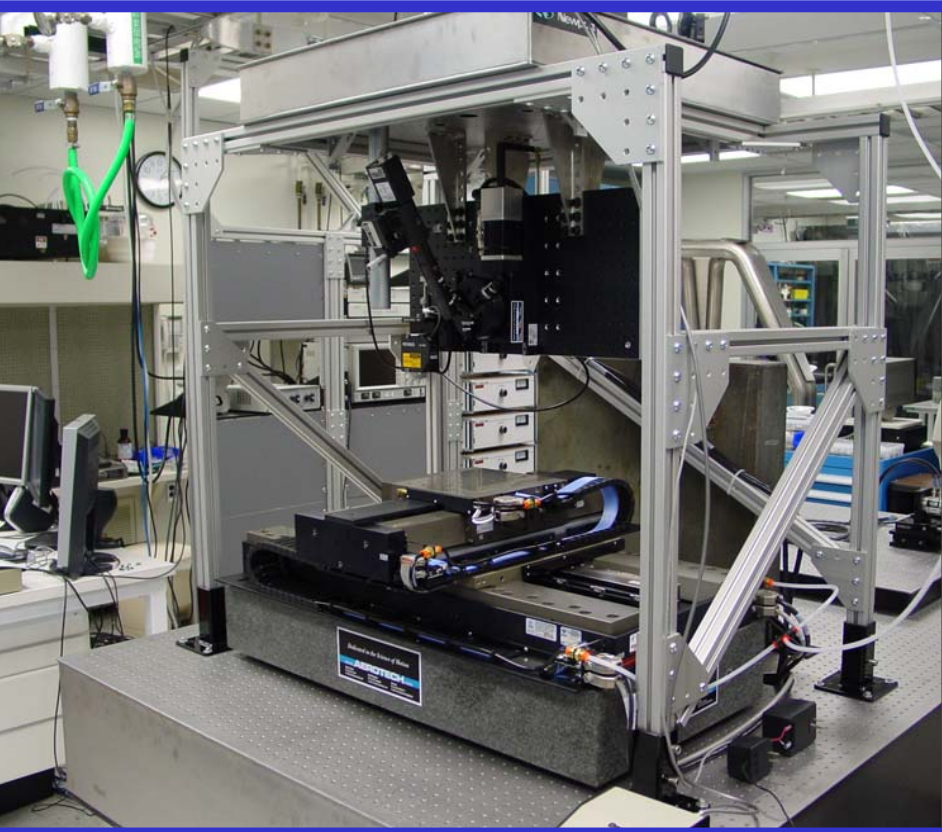
- Current Design Being Manufactured: 25% Cost Savings
- Material 304SS 4 Inch Diameter Tubing 1/10" Thick
- Weight: 359 lbs (with 100 lbs budget for optical table)
- First resonant mode: 90Hz



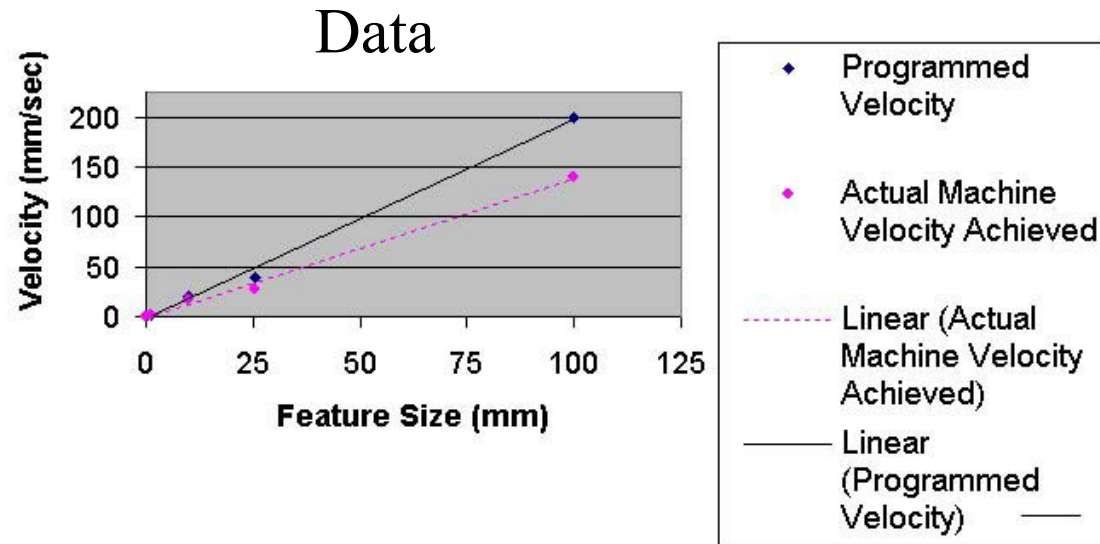
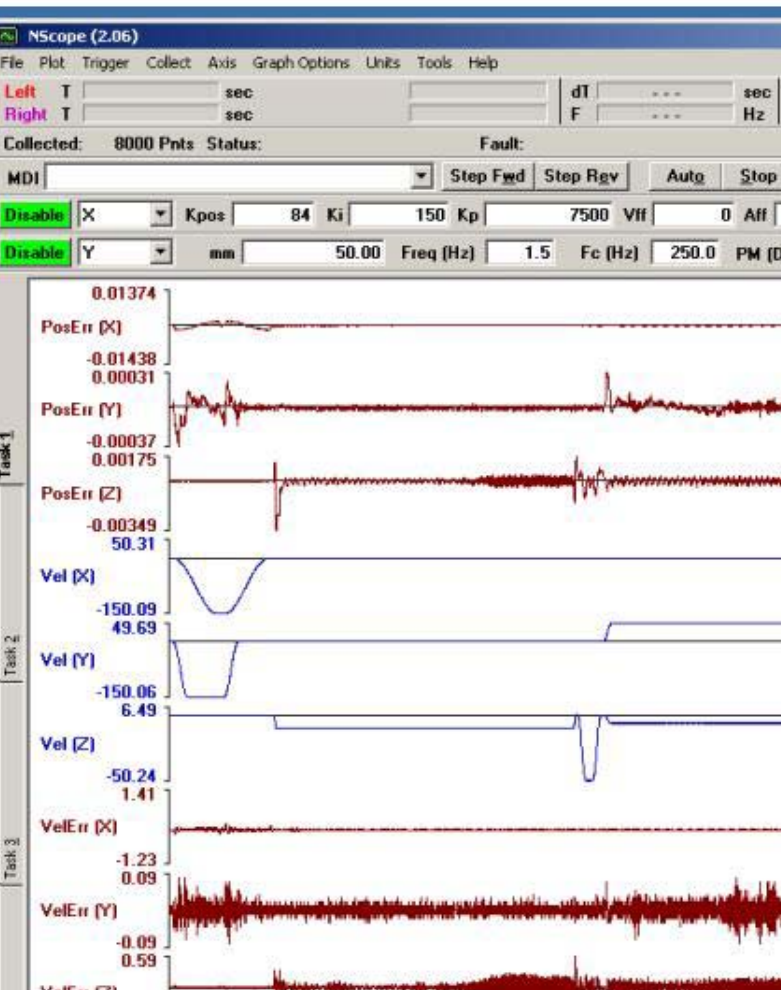
Hardware Delivered Integration Underway



XYZ Motion System



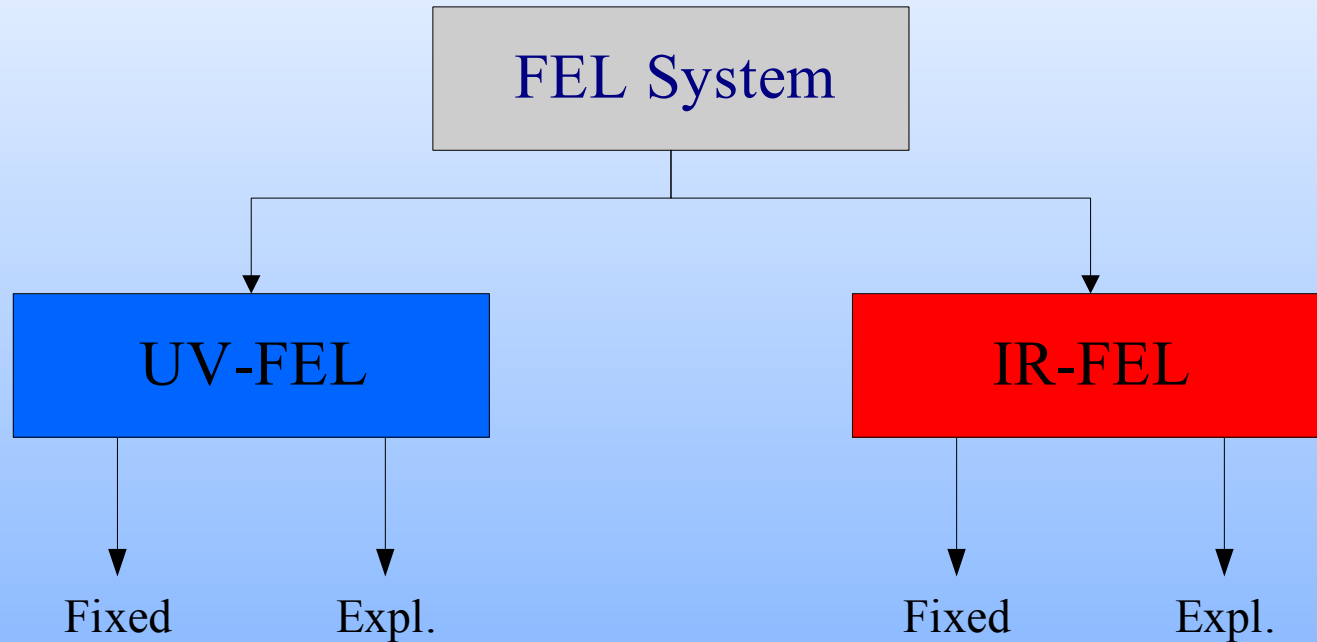
Tradeoff Between Speed and Position-Error



**For Measurements
Acceptable Upper
Limit of Position
Error Set to 200 nm**

Optical Sub System

Design Optical Configuration



2 - Fixed Optical Lines

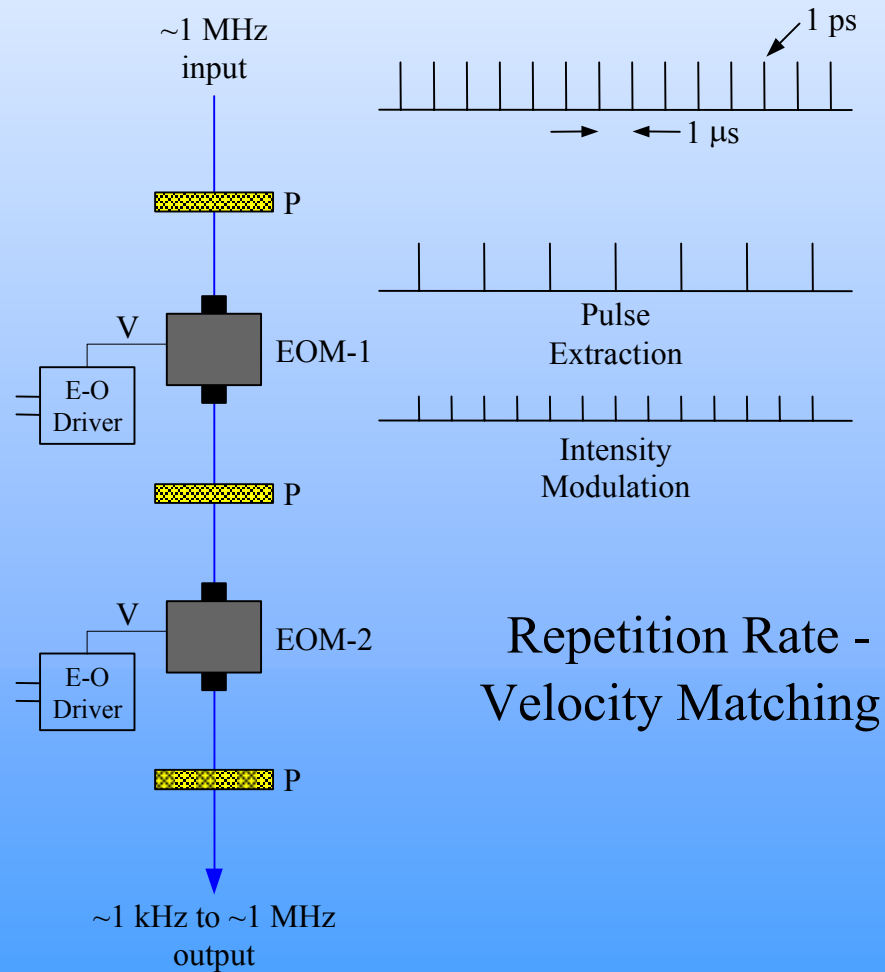
2 - Experimental Optical Lines

User-integrated components

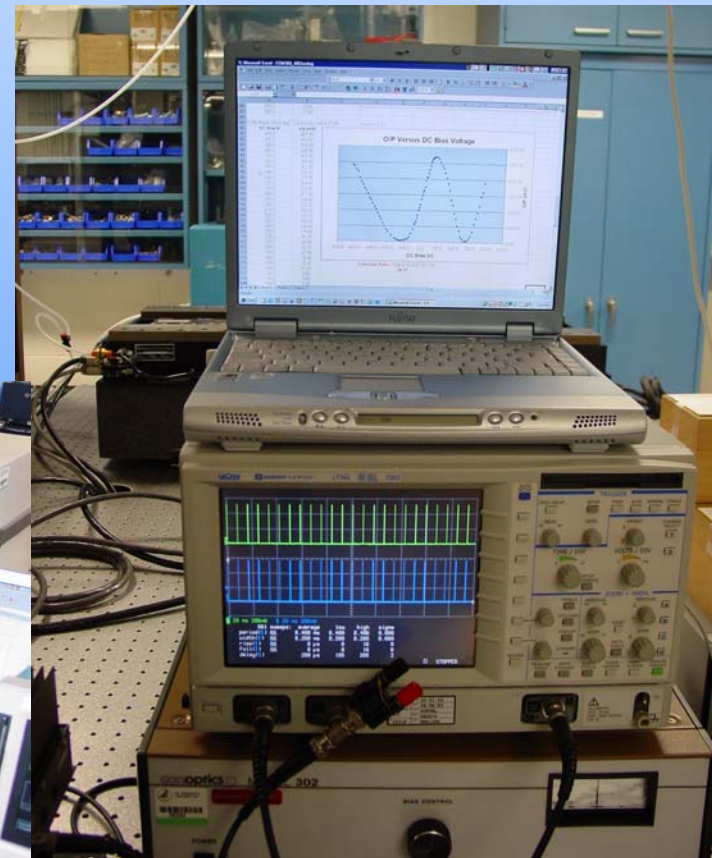
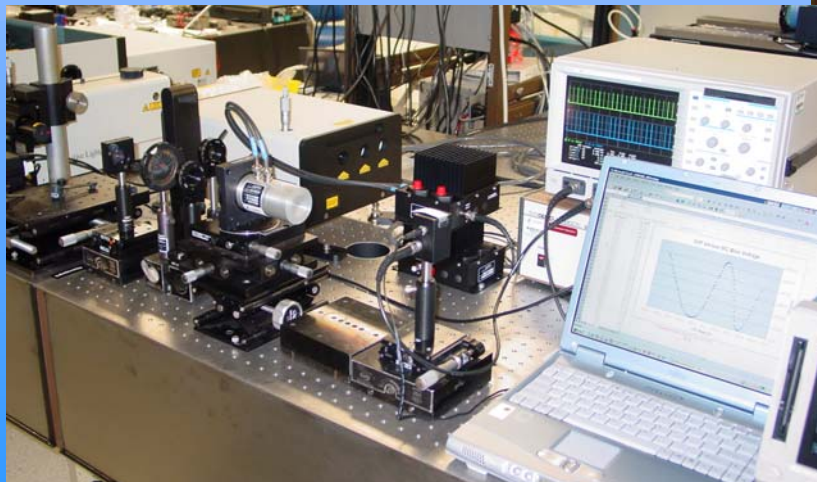
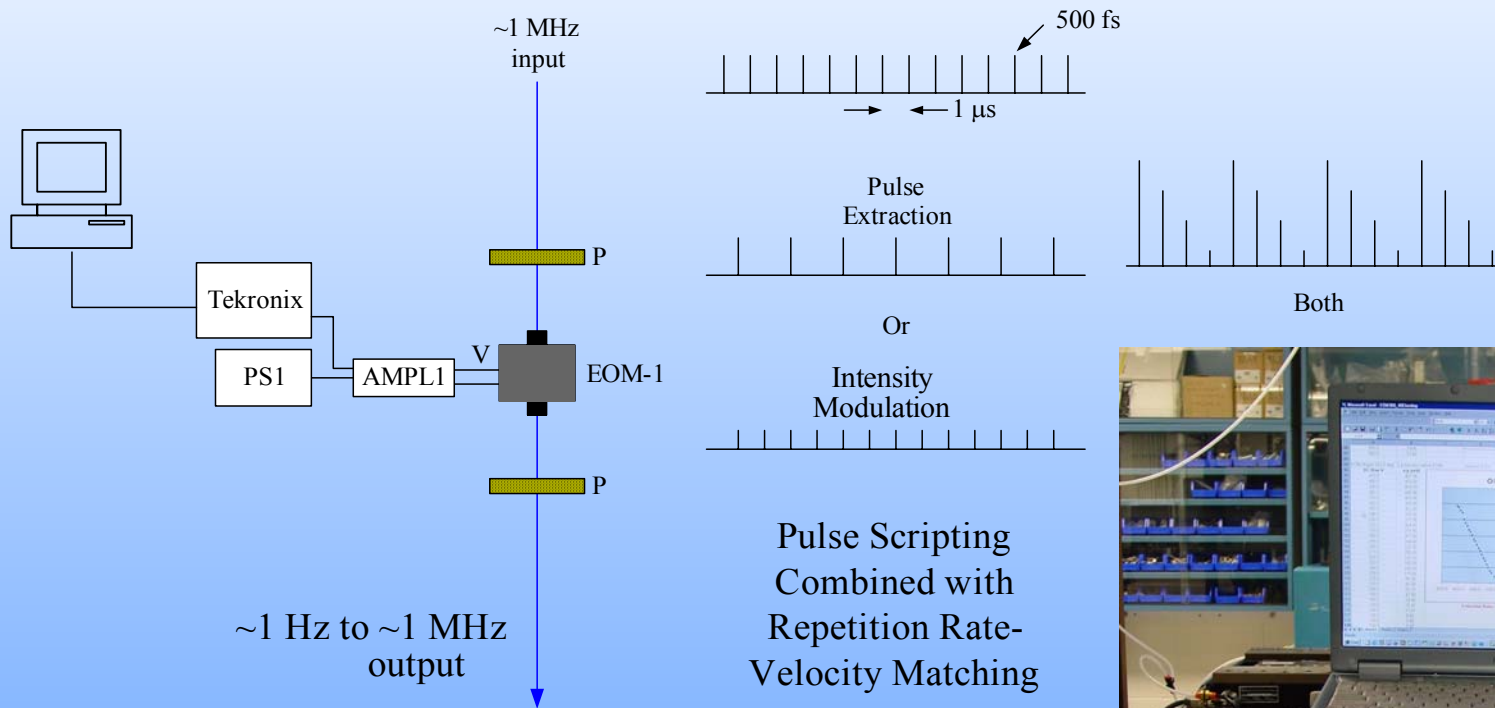
- optics
- diagnostics
- instrumentation

Pulse Picking Velocity Compensation Dynamic Control of Laser Power

Power Selection and Modulation: EOM Serial Configuration



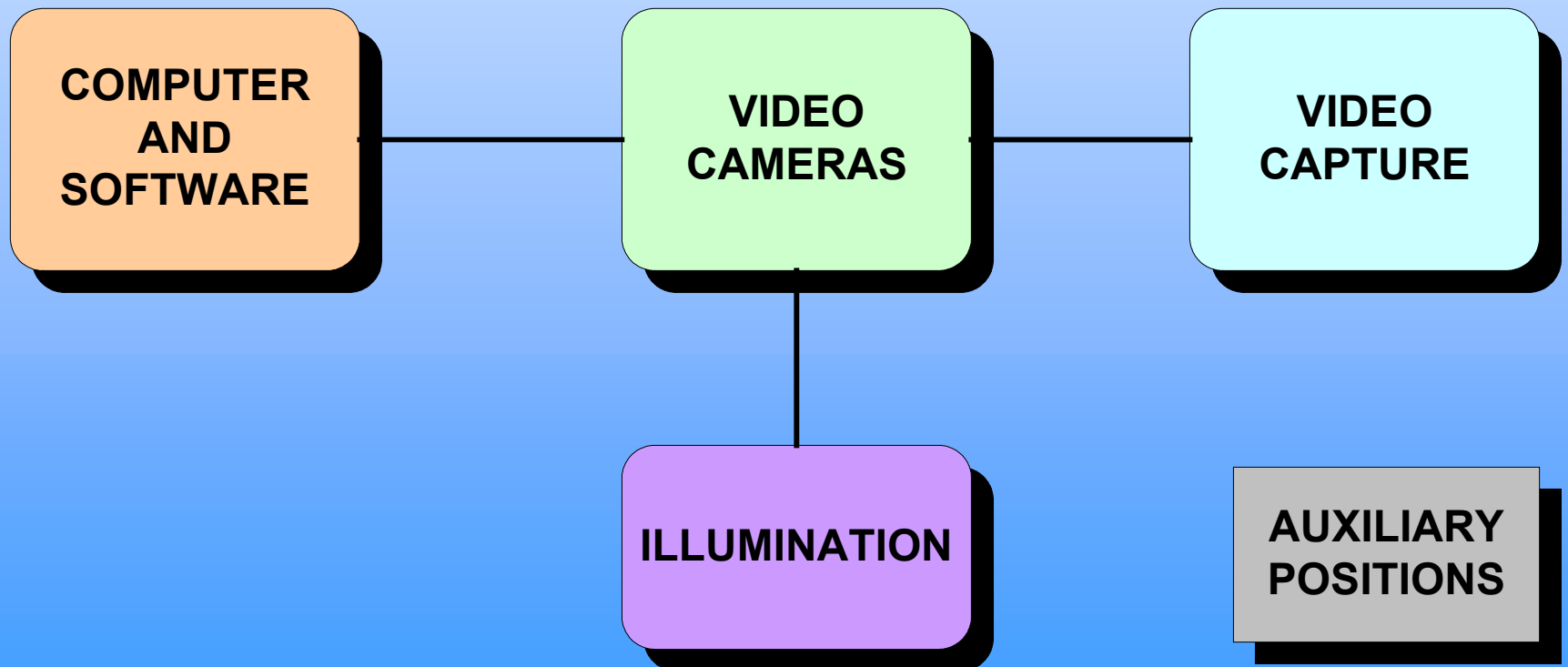
Power Selection and Modulation: EOM Serial Configuration



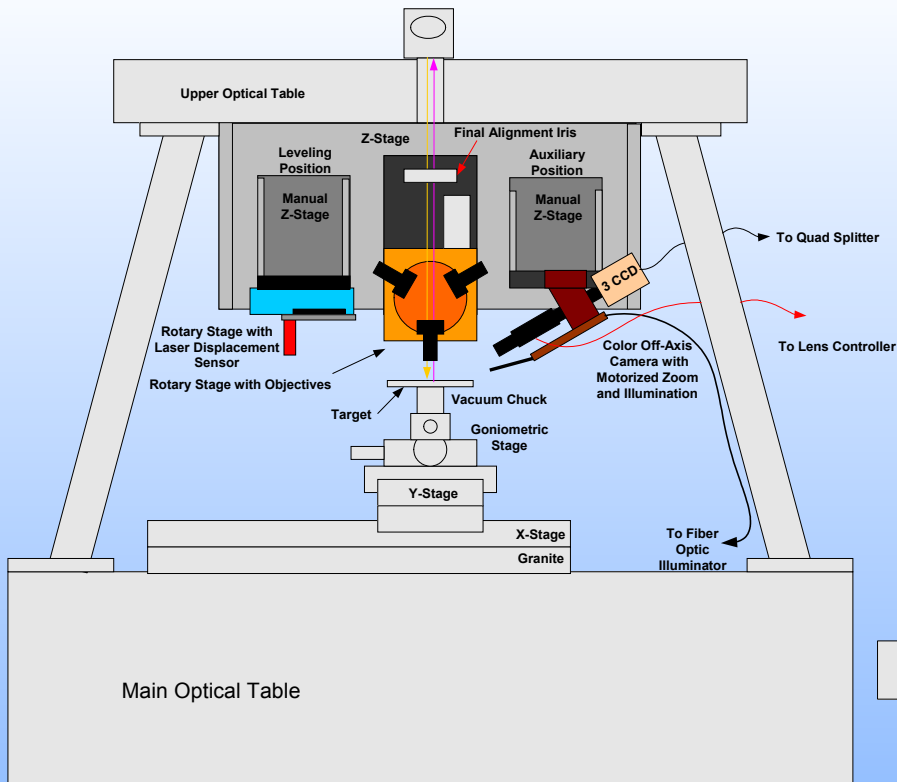
Frank.E.Livingston@aero.org

Henry.Helvajian@aero.org

Key Elements of Vision Subsystem



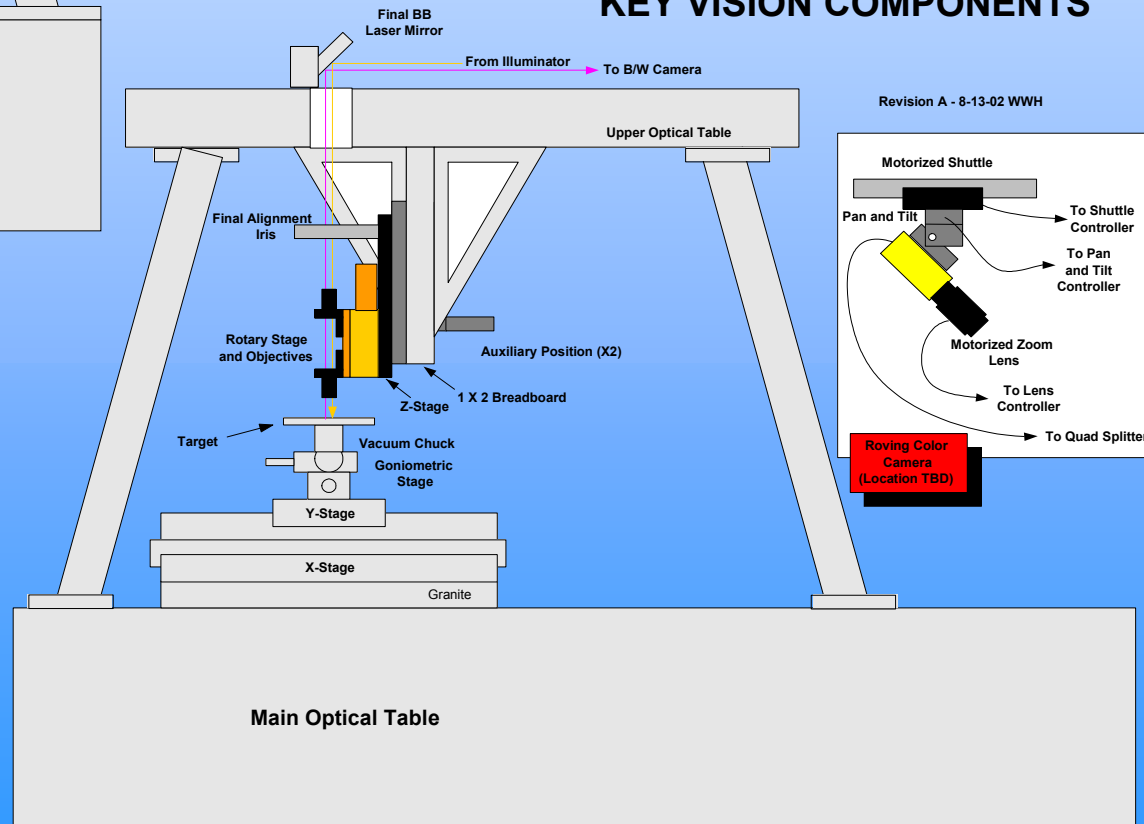
KEY VISION SYSTEM COMPONENTS



FRONT VIEW OF
MICROENGINEERING
STATION

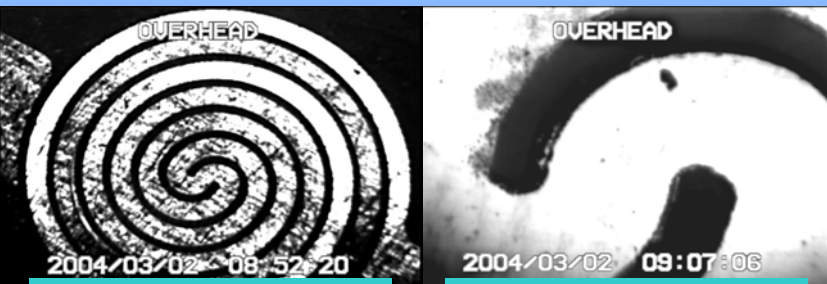
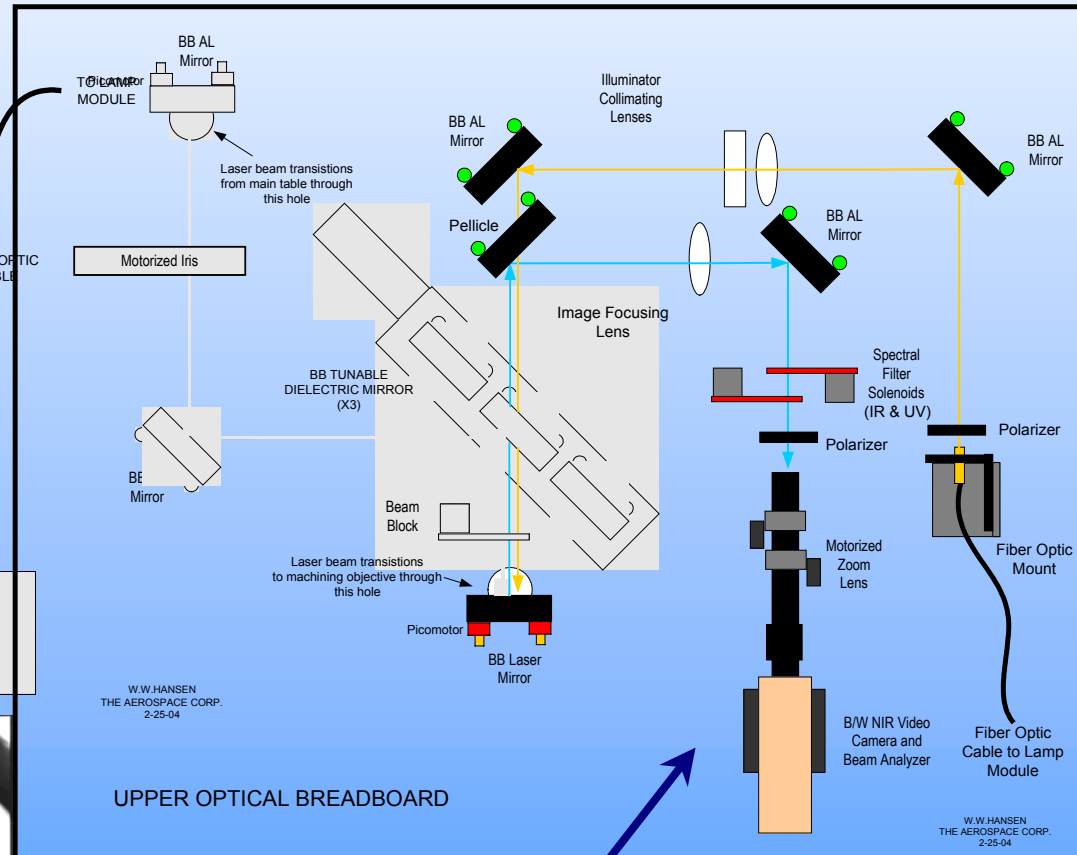
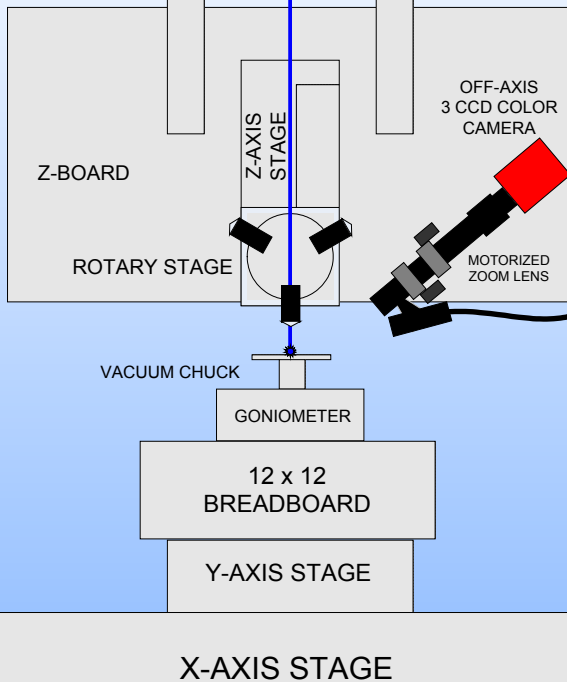
SIDE VIEW OF
MICROENGINEERING
STATION

KEY VISION COMPONENTS



UPPER OPTICAL BREADBOARD

Upper Optical Table & Vision System



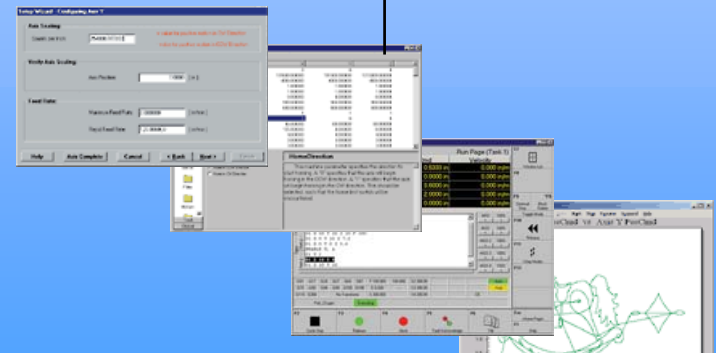
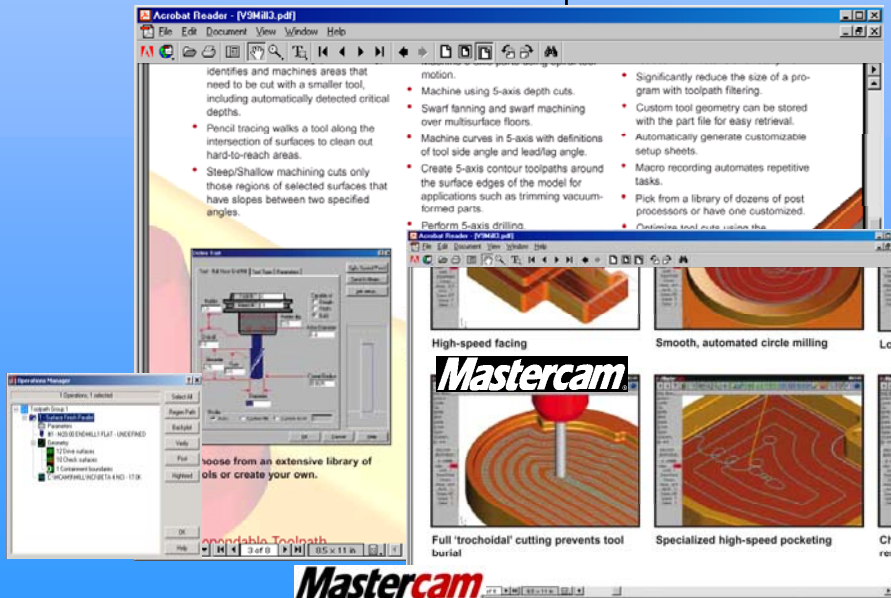
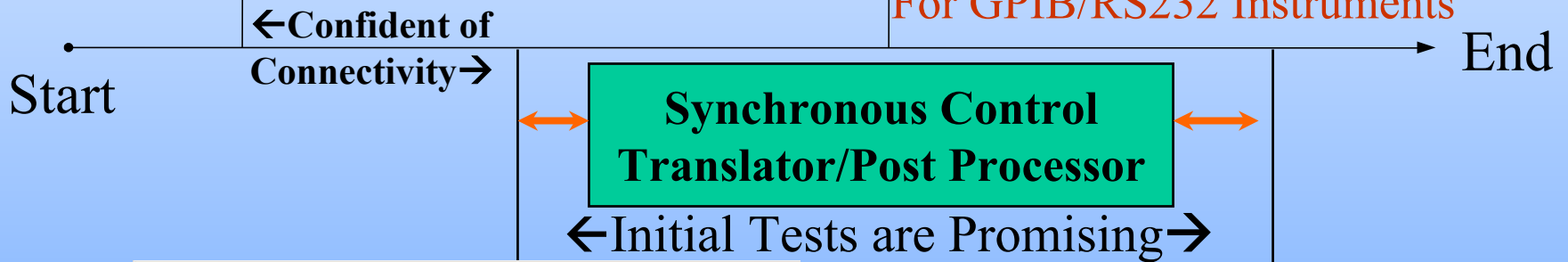
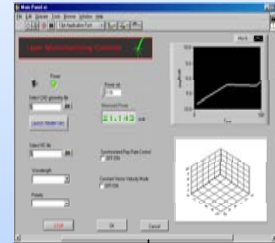
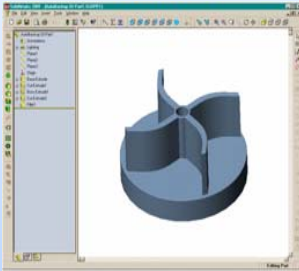
FOV 1.3mm

FOV 0.2mm

In situ laser beam analyzer for on target laser spot size and intensity distribution measurements

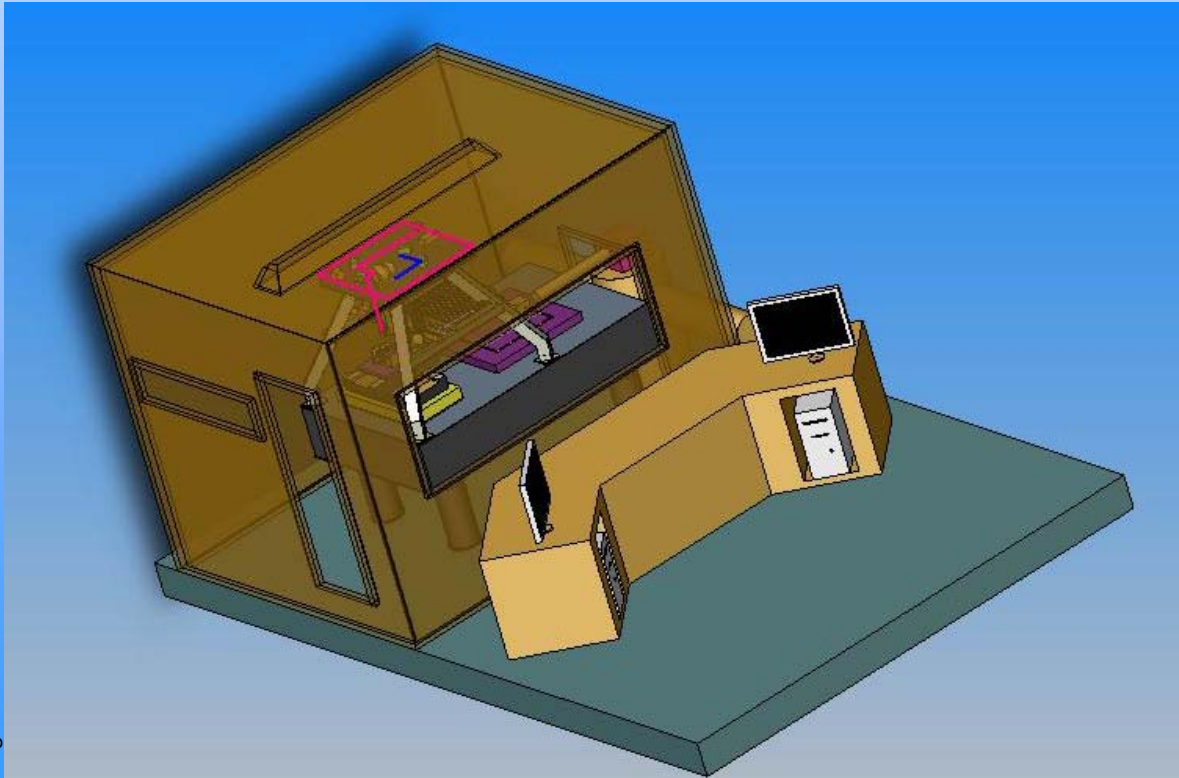
CADCAM

Software Module Sequences

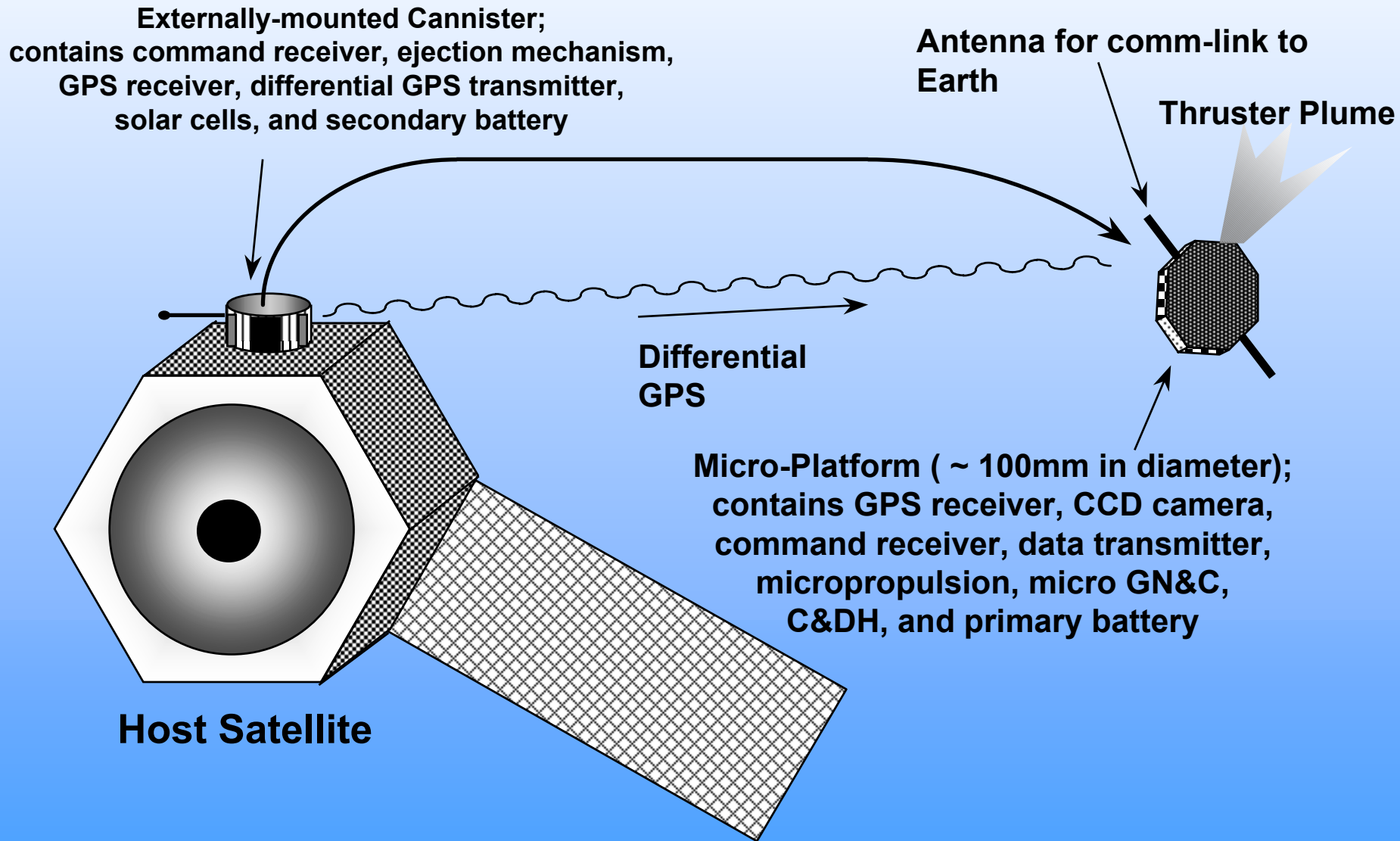


Conclusions

- Have assembled several test ‘stands’ and have investigated design properties of critical subsystems,
- Engineering Model testing underway,
- Hope to Deliver JLAB Unit Spring/Summer 2005



The Co-Orbiting Satellite Assistant (COSA)



COSA Observation Trajectories

Co-orbital with Inclination:

$$F\delta t = m \Delta v$$

$$\Delta v = 1\text{mN}(1\text{s})/0.1\text{Kg}$$

$$\Delta v = 0.01\text{m/sec}$$

Phasing orbit (Δv):

- 1st impulse: 0.003m/s
- 2nd impulse: 0.003m/s
- 700 km orbit
- 99 minute/orbit
- mN thrust levels

Observation orbits (Δv):

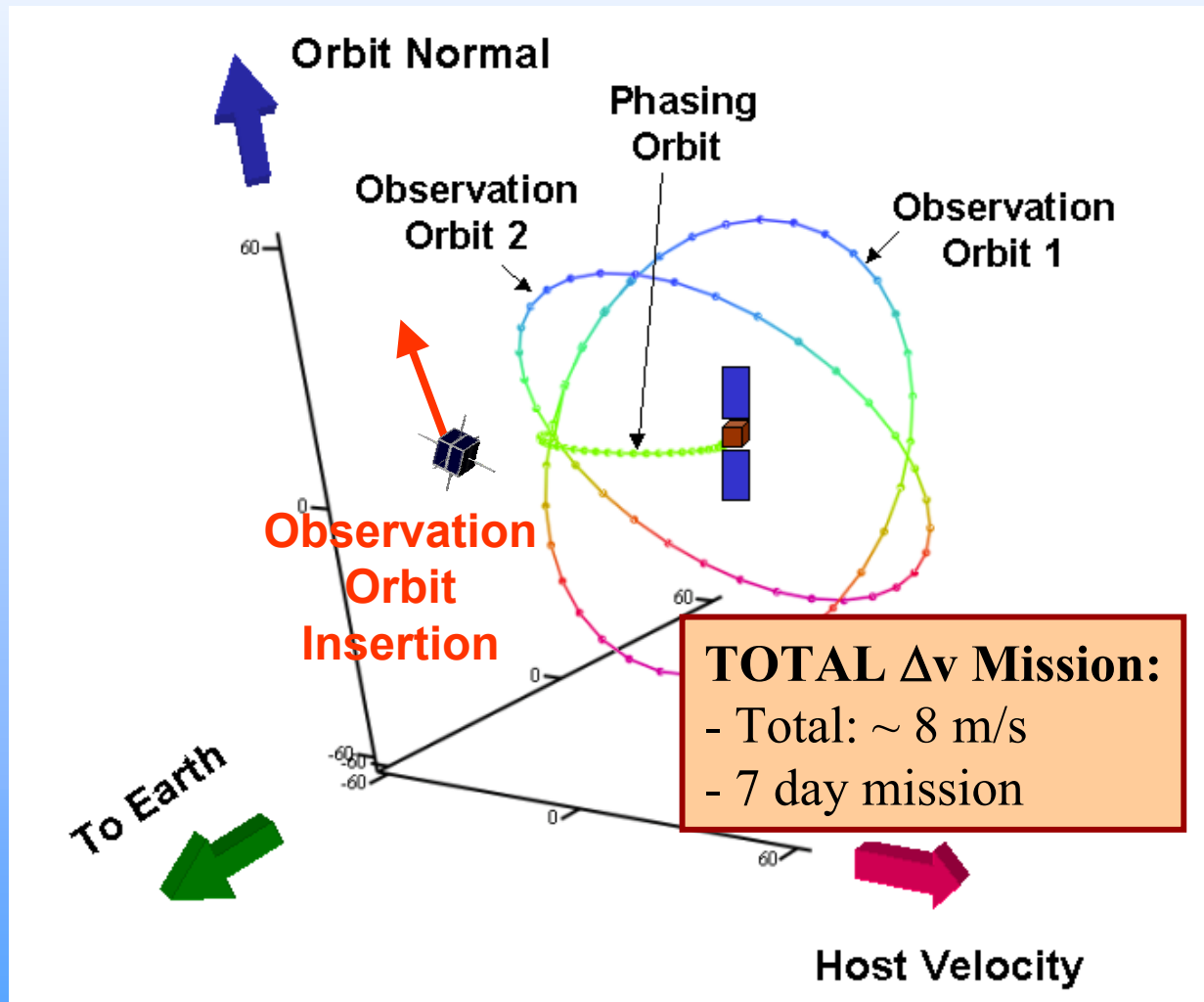
- Total: ~0.18 m/s

Atmospheric Drag(Δv):

- Total: ~7 m/s

De-orbit (Δv):

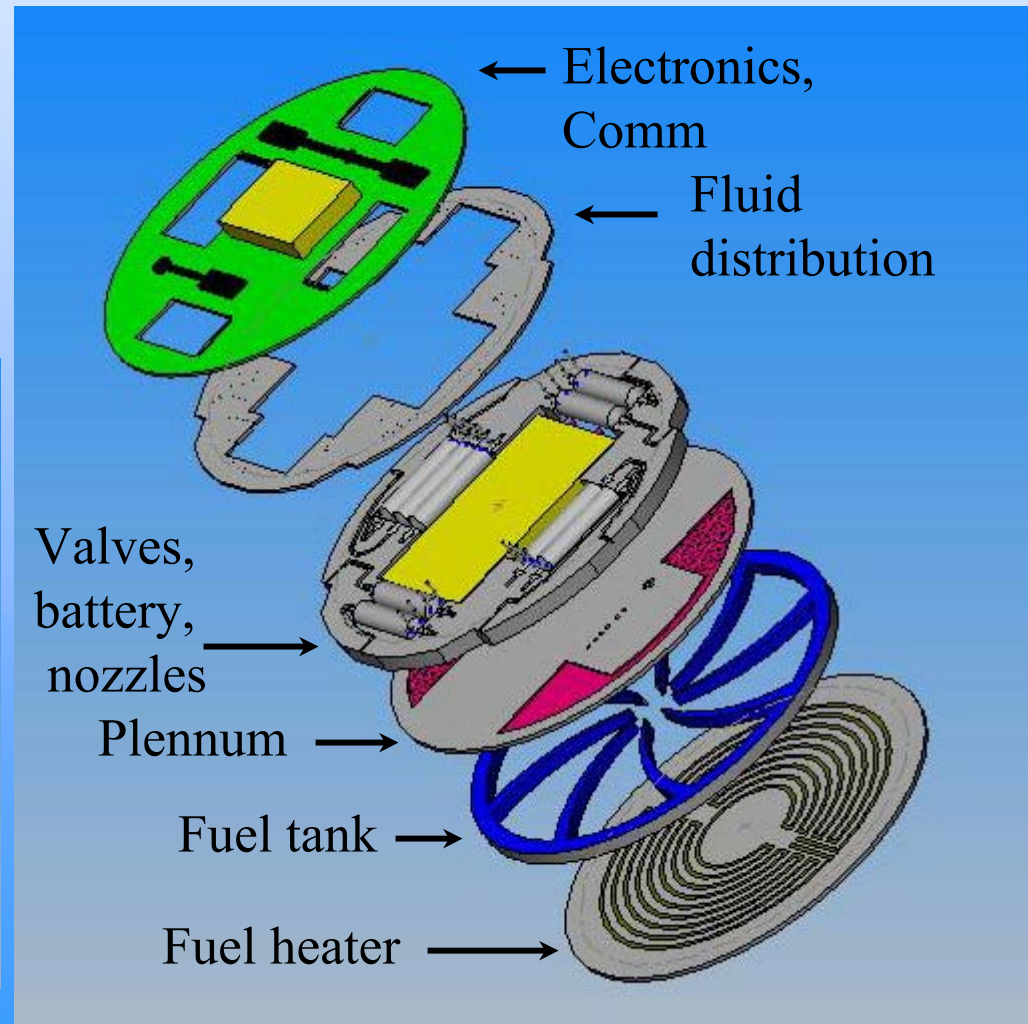
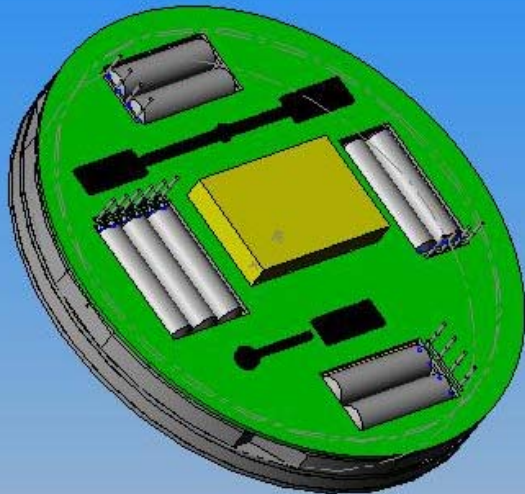
- Total: ~0.17 m/s



CO-Orbiting Satellite Assistant (COSA)

- Status
 - Vehicle design is complete
 - 9cm dia x 1cm thick
 - Total weight 160 gm
 - Mission 1 week
 - Disposable satellite
 - Fabrication to begin in April.

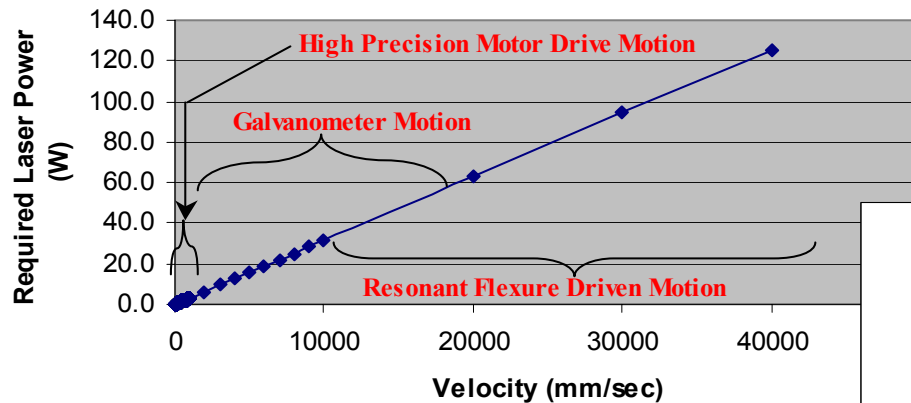
8 thrust vector nozzles



Exposure Time & Required Power: An Illustrative Case Study

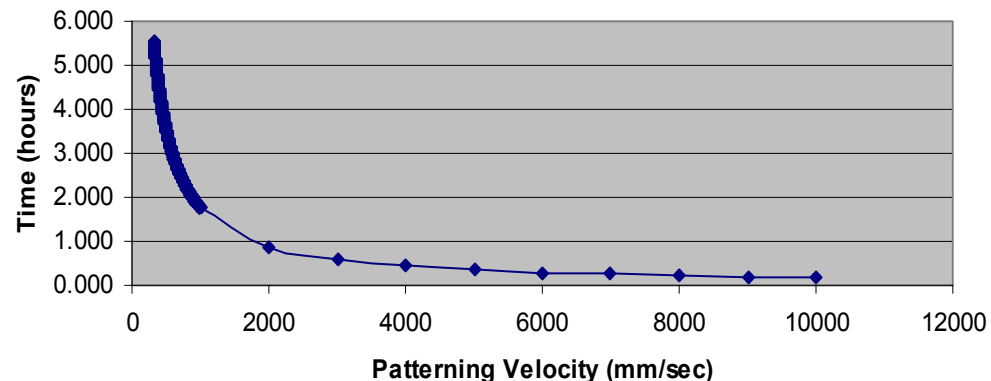
For laser wavelength of 355nm, a spot size of 2 μ m and patterning speed of 1mm/sec, A minimum laser irradiance (I) of 1mw/ μ m² is needed to obtain the maximum etch rate (@ 266nm, I ~ 0.2 mw/ μ m²)

Minimum Laser Power for Maximum Chemical Etching Contrast
as a Function of Patterning Velocity
(Laser Spot Size Dia 2 microns. Laser Wavelength 355nm)



For 266nm Laser Wavelength the Required Laser Power is a factor of 5 less, but the penetration depth is ~350 μ m

Total Exposure Time to Completely "Paint" a 100mm Square
Sample with 2 Micron Spot Size Resolution
(Laser Wavelength 355 nm)



Processing Examples
Based on Data from
Existing PSGC Material

Manufacturing Type Scenarios

Using Digital Scripted Processing of PSGC Materials

Using a Direct-Write Scheme

- Small Intranet Linked Workstations
 - Integration of a bench top microscope, with a nominal XYZ motion system coupled with a miniature femtosecond laser for small-scale 3D exposure patterning.
- High Throughput and Very Large Area Manufacturing Facility.
 - Up to KW of UV pulsed laser light,
 - With 250W incident UV laser light,
 - A processing speed of 10 meters/sec,
 - 11 μm diameter spot size,
 - A 100 mm square surface is completely patterned or “painted” in under 2 minutes.

microscope



Fs fiber laser



+



DOE – Jefferson Laboratory Free Electron Laser Processing Facility

Adam Huang

Frank Livingston

Bill Hansen

Dan Harps

Thank You

Lee Steffeney

Pete Fuqua

Dave Taylor

Meg Abraham

Seigfried Janson

Henry Helvajian